

TOUCANS

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TOUCANS

T - Third

O - Order moments (TOMs)

U - Unified

C - Condensation

A - Accounting and

N - N-dependent

S - Solver (for turbulence and diffusion)

Reynolds-averaged basic equations:

$$\frac{D\bar{u}}{dt} = S_u \overline{\frac{\partial u'w'}{\partial z}}$$

$$\frac{D\bar{v}}{dt} = S_v \overline{\frac{\partial v'w'}{\partial z}}$$

$$\frac{D\overline{S_{sL}}}{dt} = S_{S_{sL}} \overline{\frac{\partial S_{sL}'w'}{\partial z}}$$

$$\frac{D\overline{q_t}}{dt} = S_{q_t} \overline{\frac{\partial q_t'w'}{\partial z}}$$

(u , v , w - wind components, S_x - external source terms, $\frac{D()}{dt} = \frac{\partial()}{\partial t} + \bar{u}\frac{\partial()}{\partial x} + \bar{v}\frac{\partial()}{\partial y}$, $\bar{()}$ - average, $()'$ - fluctuation, z - height, t - time)

Turbulent fluxes

- $\overline{w'u'} = -K_M \frac{\partial \bar{u}}{\partial z},$
 $\overline{w'v'} = -K_M \frac{\partial \bar{v}}{\partial z}$
- $\overline{w's_{sL}'} = -K_H \frac{\partial \bar{s}_{sL}}{\partial z} + \text{TOMs terms},$
 $\overline{w'q_t'} = -K_H \frac{\partial \bar{q}_t}{\partial z} + \text{TOMs terms}$
- $\overline{w'\psi'} = C_\psi \sqrt{u^2 + v^2} (\psi - \psi_s)$ - surface layer

$K_{M/H}$ - turbulent exchange coefficients for momentum and heat and moisture, C_ψ - drag coefficient, ψ - diffused variable, $(\)_s$ - variable at surface layer

Exchange coefficients

$$K_M = \frac{\nu^4}{C_\epsilon} \chi_3(\Pi) \sqrt{e_k} L, \quad K_H = C_3 \frac{\nu^4}{C_\epsilon} \phi_3(\Pi) \sqrt{e_k} L$$

free parameters
stab. functions

given by
turbulence scheme

$$e_k(C), e_t \\ \Pi = e_t/e_k - 1$$

prognostic
turbulence energies

length scale

quasi-independent,
may depend on
TKE and BVF

$\chi_3(Ri_f), \phi_3(Ri_f)$ - stability functions, ν - free parameter, C_3 - inverse Prantl number at

neutrality, L - length scale

Framework of stability dependency functions:

- based on second order moments equations
- simple and flexible emulation of variety of turbulent schemes:
 - comparison of schemes
 - physics ensemble modeling
- properties of χ_3, ϕ_3 (Bašták, Geleyn, and Váňa, 2014):
 - valid for whole range of Ri
 - no existence of critical $Ri - Ri_{cr}$
 - anisotropy of turbulence:
 - $\frac{\partial \chi_3}{\partial Ri} \neq 0, \frac{\partial \phi_Q}{\partial Ri} \neq 0$

(Ri -gradient Richardson number, ϕ_Q - non - energy conversion part of ϕ_3 - coefficient)

Framework of stability dependency functions:

- simple shape in terms of Ri_f :

$$\chi_3(Ri) = \frac{1 - \frac{Ri_f}{R}}{1 - Ri_f}, \quad \phi_3(Ri) = \frac{1 - \frac{Ri_f}{P}}{1 - Ri_f},$$

$$\phi_Q(Ri) = \frac{1 - \frac{Ri_f}{Q}}{1 - Ri_f}, \quad \frac{Ri}{Ri_f} = \frac{P(R - Ri_f)}{C_3 R (P - Ri_f)}$$

$$0 < \lim_{Ri \rightarrow \infty} P = Ri_{fc} < 1, \quad Ri_{fc} < \lim_{Ri \rightarrow \infty} R \equiv R_\infty \leq 1, \quad Ri_{fc} \leq \lim_{Ri \rightarrow \infty} Q \equiv Q_\infty \leq 1.$$

- factorization of $\phi_3(Ri)$:

$$\phi_3 = \underbrace{\phi_Q(Ri)}_{\text{anisotropy}} \underbrace{\left(1 - \frac{2 O_\lambda (e_t - e_k)}{C_4 w'^2}\right)}_{\text{energy conversion}}, \quad \frac{\partial \phi_Q}{\partial Ri} \neq 0$$

($Ri_f = Ri K_H / K_M$ -flux Richardson number, O_λ -free parameter, C_4 - coefficient)

Framework of stability functions:

- the turbulent scheme then depends on:
 - 4(3) free parameters
 - ν - overall turbulence intensity,
 - C_ϵ - turbulent energy dissipation
 - following Schmidt and Schumann (1989)
 - we assume: $C_\epsilon = \pi \nu^2$,
 - C_3 -inverse Prandtl number at neutrality,
 - O_λ - TKE ↔ TPE conversion,
 - 3 “functional dependencies” (P , R , Q)

	Model I	Model II	eeQNSE	eeEFB
P	Const.	Const.	Const.	Ri fun.
R	Const.	Const.	Ri fun.	Ri fun.
Q	Const.	Ri fun.	Ri fun.	Ri fun.

Emulation and extension of turbulent schemes:

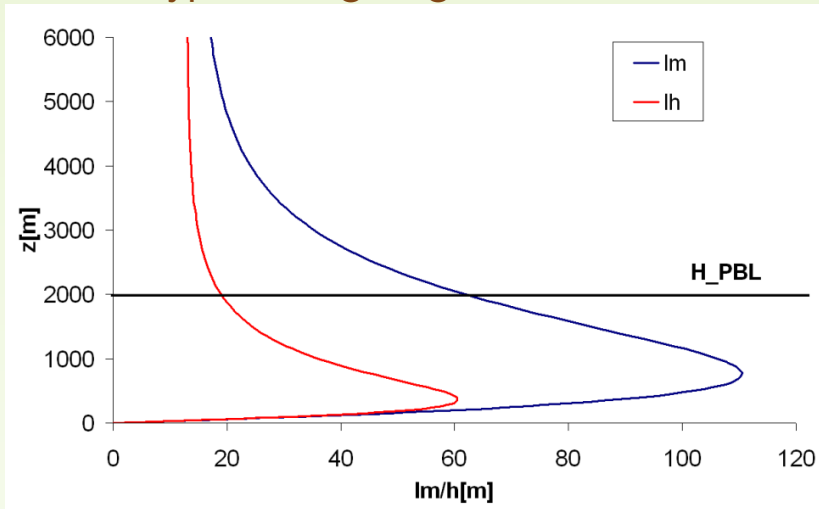
- turbulent schemes without Ri_{cr} can be emulated in BGV2014 framework
- continuous extension to unstable regime ($Ri < 0$) is required for schemes that are defined only in stable regime ($Ri > 0$)
- eeQNSE = emulation and extension of Quasi Normal Scale Elimination (QNSE) scheme - Sukoriansky et al. (2005)
- eeEFB = emulation and extension of Energy- and Flux-Budget (EFB) scheme - Zilitinkevich et al. (2013)

Prandtl-type mixing lengths l_m and l_h
(CGMIXLEN='AY', in ALARO0='CG') :

$$l_{m/h}^{GC} = \frac{\kappa Z}{1 + \frac{\kappa Z}{\lambda_{m/h}} \left[\frac{1 + \exp\left(-a_{m/h} \sqrt{\frac{z}{H_{pbl}} + b_{m/h}}\right)}{\beta_{m/h} + \exp\left(-a_{m/h} \sqrt{\frac{z}{H_{pbl}} + b_{m/h}}\right)} \right]}$$

(κ is Von Kármán constant, z is height, $a_{m/h}$, $b_{m/h}$, $\beta_{m/h}$ and $\lambda_{m/h}$ are tuning constants and H_{pbl} is PBL height)

Prandtl-type mixing lengths:



TKE based length scales L

- Bougeault a Lacarrère (1989) :

$$L_{BL}(E) = \left(\frac{L_{up}^{-\frac{4}{5}} + L_{down}^{-\frac{4}{5}}}{2} \right)^{-\frac{5}{4}}$$

$L_{up}(E)$ ($L_{down}(E)$) - L upward (downward)

- $L_N = \sqrt{\frac{2 \cdot E}{N^2}}$ for stable stratification
- with possibility to use moist BVF
- possible prognostic treatment of L

Conversion between L and l_m

- following RMC01:

$$L_K = \frac{C_\epsilon}{\nu^3} l_m \frac{f(Ri)^{\frac{1}{4}}}{\chi_3^{\frac{1}{2}}}, \quad L_\epsilon = \frac{C_\epsilon}{\nu^3} l_m \frac{\chi_3^{\frac{3}{2}}}{f(Ri)^{\frac{3}{4}}}$$

- assuming: $L \equiv (L_K^3 L_\epsilon)^{\frac{1}{4}}$ we get:

$$L = \frac{C_\epsilon}{\nu^3} l_m$$

Third Order Moments (TOMs)

- parametrization for heat and moisture
- following (Canuto, Cheng, and Howard, 2007):

$$\overline{w'\theta'} = -K_H \frac{\partial \bar{\theta}}{\partial z} + A_1^\theta \frac{\partial \overline{w'^3}}{\partial z} + A_2^\theta \frac{\partial \overline{w'\theta'^2}}{\partial z} + A_3^\theta \frac{\partial \overline{w'^2\theta'}}{\partial z}$$

$$\overline{w'^3} = -0.06 \frac{g}{\theta} \tau^2 \overline{w'^2} \frac{\partial \overline{w'\theta'}}{\partial z}, \quad \overline{w'\theta'^2} = -\tau \overline{w'\theta'} \frac{\partial \overline{w'\theta'}}{\partial z}, \quad \overline{w'^2\theta'} = -0.3 \tau \overline{w'^2} \frac{\partial \overline{w'\theta'}}{\partial z}$$

$A_1^\theta, A_2^\theta, A_3^\theta$ - coefficients, τ - dissipation time scale

- two step solver: local + non-local correction

Prognostic TTE/TPE

- based on Zilitinkevich et al.(2013)
- addition of second prognostic turbulent energy:
Turbulent Potential Energy (TPE), or
 $TTE = TKE + TPE$
- consideration of counter-gradient heat transport
maintained by velocity shear in very stable stratification
- stability parameter based on energy ratio $\Pi = TPE/TKE$
(linked to fluxes) rather than on local gradients (Ri)

Prognostic TKE- e_k , TPE- e_p eqs.:

- based on Zilitinkevich et al.(2013)

$$\frac{de_k}{dt} = -g \frac{\partial}{\partial p} \left(\rho K_{e_k} \frac{\partial e_k}{\partial z} \right) + I + II - \frac{2 e_k}{\tau_k}$$

$$\frac{de_p}{dt} = -g \frac{\partial}{\partial p} \left(\rho K_{e_p} \frac{\partial e_p}{\partial z} \right) - II - \frac{2 e_p}{\tau_p}$$

$$\tau_p \equiv \tau_k \frac{C_4}{2 C_3}$$

(I , II - shear and buoyancy source terms, K_{e_k} , K_{e_t} - turbulent exchange coefficients for TKE and TTE, τ_k , τ_p , τ_t - dissipation time scale for TKE, TPE and TTE, Π - stability parameter, C_3 - inverse Prandtl number at neutrality, C_4 - coefficient, p - pressure, g - acceleration of gravity, ρ - density)

Prognostic TTE - $e_t = e_k + e_p$ equation:

$$\frac{de_t}{dt} = -g \frac{\partial}{\partial p} \left(\rho K_{e_t} \frac{\partial e_t}{\partial z} \right) + I - \frac{2 e_t}{\tau_t}$$

$$\tau_t \equiv \tau_k \frac{C_4 (1 + \Pi)}{C_4 + 2 C_3 \Pi},$$

$$Ri_f = \frac{\Pi}{\frac{C_4}{2 C_3} + \Pi}$$

(e_p - TPE, K_{e_t} - turbulent exchange coefficient for TTE, τ_t - dissipation time scale for TTE, $Ri_f = Ri K_H/K_M$ - flux Richardson number, C_4 - coefficient)

Dry versus moist case:

- dry:

$$H_d = \frac{g}{\theta} \overline{\theta' w'}, \quad e_{pd} = \frac{g}{\theta} \frac{\overline{\theta'^2}}{2 \frac{\partial \theta}{\partial z}}$$

- moist:

$$H_m = \frac{g}{\rho_0} \overline{w' \rho'} = E_{s_{sL}} \overline{w' s_{sL}'} + E_{q_t} \overline{w' q_t'}$$

$$e_{pm} = \frac{E_{sL} \overline{s_{sL}'^2}}{2 \frac{\partial s_{sL}}{\partial z}} + \frac{E_{q_t} \overline{q_t'^2}}{2 \frac{\partial q_t}{\partial z}}$$

- E_{sL} , E_{q_t} are derived after (Marquet and Geleyn, 2013) and depend on cloud fraction C and skewness parameter C_n

$$E_{sL} = \frac{g M(C)}{\bar{c}_p \bar{T}},$$

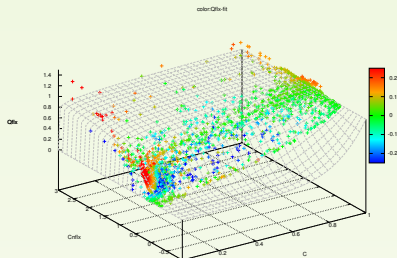
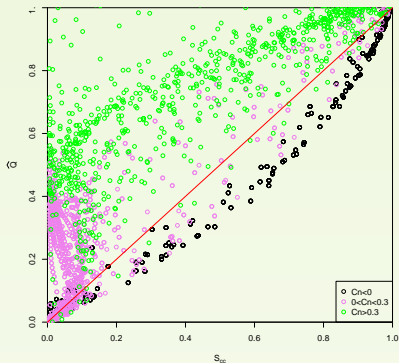
$$E_{qt} = g M(C) \left\{ \left(\frac{R_v - R_d}{R_d \cdot \bar{q}_d + R_v \cdot \bar{q}_v} - \frac{c_{pv} - c_{pd}}{\bar{c}_p} \right) + \hat{Q} \left[\frac{L_{vs}(\bar{T})(R_d \cdot \bar{q}_d + R_v \cdot \bar{q}_v)}{\bar{c}_p \bar{T} R_v} - 1 \right] \cdot \left[\frac{R_v - R_d}{R_d \cdot \bar{q}_d + R_v \cdot \bar{q}_v} + \frac{1}{(1 - q_t)(1 + D_C)} \right] \right\}$$

$$\left(M(C) = \frac{1 + D_C}{1 + D_C \left(1 + C \left[\frac{L_{vs}(\bar{T})(R_d \cdot \bar{q}_d + R_v \cdot \bar{q}_v)}{\bar{c}_p \bar{T} R_v} - 1 \right] \right)}, D_C = \frac{L_{vs}(\bar{T}) r_s^{\text{li}}}{R_d \bar{T}} = \frac{\bar{T}}{\bar{p} - e_{\text{sat}}(\bar{T})} \frac{\partial e_{\text{sat}}(\bar{T})}{\partial \bar{T}} \right)$$

$$\widehat{Q} = C^{F(C_n)}, \quad F(C_n) = 0.5 \left[\sqrt{(6.25 C_n)^2 + 4} - 6.25 C_n \right]$$

$$C_n = \frac{-\frac{\overline{w' s'_{sl}}}{c_p \overline{T}} - \left(\frac{R_v - R_d}{R_d \cdot \widehat{q}_d + R_v \cdot \widehat{q}_v} - \frac{c_{pv} - c_{pd}}{\widehat{c}_p} \right) \overline{w' q'_t}}{\left[\frac{L_{vs}(\widehat{T})(R_d \cdot \widehat{q}_d + R_v \cdot \widehat{q}_v)}{c_p \widehat{T} R_v} - 1 \right] \left[\frac{R_v - R_d}{R_d \cdot \widehat{q}_d + R_v \cdot \widehat{q}_v} + \frac{1}{(1 - \widehat{q}_t)(1 + D_C)} \right] \overline{w' q'_t}}$$

Fitting of $\hat{Q}(C, C_n)$ on LES data (courtesy of D. Lewellen)



Summary

- TOUCANS is a complex and flexible framework for turbulence parametrization
- TOUCANS contains several novel or specific approaches to parametrization of turbulence
- TOUCANS was developed as part of ALARO, and therefore interactions with other parametr. are possible
- TOUCANS is far from finished, there are many experimental branches

Thank you for your attention